

## Claims

1. A circuit arrangement, for generating an x-ray  
5 tube voltage, comprising:  
an inverse rectifier circuit ( $G_{si}$ ) for generating  
a  
high-frequency alternating voltage,  
a high-voltage generator ( $G_{su}$ ) for converting the  
10 high-frequency alternating voltage into a high voltage for  
the x-ray tube ,  
a voltage controller ( $G_{RU}$ ), which based on a  
deviation of an x-ray tube voltage ( $V_U(t)$ ) from a set-point  
x-ray tube voltage ( $W_{U(t)}$ ) generates a first controlling  
15 variable value ( $Y_{U(t)}$ ) for the inverse rectifier circuit  
( $G_{si}$ ),  
a measurement circuit for measuring an  
oscillating current ( $i_{sw(t)}$ ) applied to one output of the  
inverse rectifier circuit ( $G_{si}$ ) of the high-frequency  
20 alternating voltage,  
an oscillating current controller ( $G_{RI}$ ), which  
based on a deviation of an ascertained actual oscillating  
current value ( $V_I(t)$ ) from a predetermined maximum  
oscillating current value ( $W_{I_{max}}$ ) generates a  
25 second controlling variable value ( $Y_{I(t)}$ ) for the inverse  
rectifier circuit ( $G_{si}$ ), and wherein  
a switching device, connected downstream of the  
voltage controller ( $G_{RU}$ ) and the oscillating current  
controller ( $G_{RI}$ ), operable to compare the first controlling  
30 variable value ( $Y_{U(t)}$ ) and the second controlling variable  
value ( $Y_{I(t)}$ ) and is operable to send the lesser of the  
first and second controlling variable values ( $Y_{U(t)}$  and  
 $Y_{I(t)}$ ) onward as a resultant controlling variable value  
( $Y(t)$ ) to the inverse rectifier circuit ( $G_{si}$ ).

2. The circuit arrangement as of claim 1, wherein  
at least one of the voltage controller ( $G_{RU}$ ) and the  
oscillating current controller ( $G_{RI}$ ) includes a PI  
5 controller.

3. The circuit arrangement as of claim 1, wherein  
one output of the switching device is connected to at  
least one of the voltage controller ( $G_{RU}$ ) and of the  
10 oscillating current controller ( $G_{RI}$ ); and that the voltage  
controller ( $G_{RU}$ ) and the oscillating current controller  
( $G_{RI}$ ) are such the resultant controlling variable value  
( $Y(t)$ ) is carried along, if neither one of the controlling  
variable values ( $Y_{U(t)}$ ) and ( $Y_{I(t)}$ ) generated by their  
15 respective controllers is sent onward as the resultant  
controlling variable value ( $Y(t)$ ).

4. The circuit arrangement as of claim 2, wherein  
20 one output of the switching device is connected to at  
least one of the voltage controller ( $G_{RU}$ ) and of the  
oscillating current controller ( $G_{RI}$ ); and that the voltage  
controller ( $G_{RU}$ ) and the oscillating current controller  
( $G_{RI}$ ) are such the resultant controlling variable value  
25 ( $Y(t)$ ) is carried along, if neither one of the controlling  
variable values ( $Y_{U(t)}$ ) and ( $Y_{I(t)}$ ) generated by their  
respective controllers is sent onward as the resultant  
controlling variable value ( $Y(t)$ ).

5. The circuit arrangement as of claim 1, wherein  
the switching device is such that no controlling variable  
lower than a predetermined minimum controlling variable  
value ( $Y_{min}$ ) is sent onward as the resultant controlling  
35 variable value ( $Y(t)$ ) to the inverse rectifier circuit

(G<sub>si</sub>).

6. The circuit arrangement as of claim 4, wherein  
5 the switching device is such that no controlling variable  
lower than a predetermined minimum controlling variable  
value (Y<sub>min</sub>) is sent onward as the resultant controlling  
variable value (Y(t)) to the inverse rectifier circuit  
(G<sub>si</sub>).

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7. The circuit arrangement as of claim 1, wherein  
switching device is such that no controlling variable  
higher than a predetermined maximum controlling variable  
value (Y<sub>min</sub>) is send onward as the resultant controlling  
15 variable value (Y(t)) to the inverse rectifier circuit  
(G<sub>si</sub>).

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8. The circuit arrangement as of claim 6, wherein  
switching device is such that no controlling variable  
20 higher than a predetermined maximum controlling variable  
value (Y<sub>min</sub>) is send onward as the resultant controlling  
variable value (Y(t)) to the inverse rectifier circuit  
(G<sub>si</sub>).

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9. The circuit arrangement as of claim 1, wherein  
at least one of the voltage controller (G<sub>RU</sub>) and the  
oscillating current controller (G<sub>RI</sub>) can vary at least one  
30 parameter, the at least one parameter being a function of  
at least one of a set x-ray tube voltage (U<sub>R0</sub>) and a set x-  
ray tube current (I<sub>R0</sub>).

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10. An x-ray generator having a circuit arrangement  
35 of claims 1.

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11. An x-ray generator having a circuit arrangement of claim 8.

12. An x-ray system having an x-ray generator of claim 10.

13. A method for generating an x-ray tube voltage where a high-frequency alternating voltage is generated via an inverse rectifier circuit ( $G_{si}$ ), the high-frequency alternating voltage is converted into a high voltage for the x-ray tube via a high-voltage generator ( $G_{su}$ ), and a first controlling variable value ( $Y_{U(t)}$ ) is generated for the inverse rectifier circuit ( $G_{si}$ ) via a voltage controller ( $G_{RU}$ ) due to a deviation of an x-ray tube voltage ( $V_U(t)$ ) from a set-point x-ray tube voltage ( $W_{U(t)}$ ), the method comprising:

measuring an oscillating current ( $i_{sw(t)}$ ) via a measurement circuit that is connected to one output of the inverse rectifier circuit ( $G_{si}$ ) of the high-frequency alternating voltage,

generating a second controlling variable value ( $Y_{I(t)}$ ) for the inverse rectifier circuit ( $G_{si}$ ) via an oscillating current controller ( $G_{RI}$ ), due to a deviation of an ascertained actual oscillating current value ( $V_I(t)$ ) from a predetermined maximum oscillating current value ( $W_{I\_max}$ ),

comparing the first controlling variable value ( $Y_{U(t)}$ ) and the second controlling variable value ( $Y_{I(t)}$ ) via a switching device, the switching device being connected downstream of the voltage controller ( $G_{RU}$ ) and the oscillating current controller ( $G_{RI}$ ), and

sending the lesser of the first and second controlling variable values ( $Y_{U(t)}$  and  $Y_{I(t)}$ ) onward as a

resultant controlling variable value ( $Y(t)$ ) to the inverse rectifier circuit ( $G_{si}$ ).

5           14. The method as of claim 13, further comprising using a PI controller in at least one of the voltage controller ( $G_{RU}$ ) and the oscillating current controller ( $G_{RI}$ ).

10           15. The method as of claim 13, further comprising feeding back the resultant controlling variable value ( $Y(t)$ ) as an input value to at least one of the voltage controller ( $G_{RU}$ ) and/or to the oscillating current controller ( $G_{RI}$ ), and carrying along the resultant  
15 controlling variable value ( $Y(t)$ ), if neither one of the controlling variable values ( $Y_{U(t)}$ ) and ( $Y_{I(t)}$ ) generated by their respective controllers is sent onward as the resultant controlling variable value ( $Y(t)$ ).

20           16. The method as of claim 14, further comprising feeding back the resultant controlling variable value ( $Y(t)$ ) as an input value to at least one of the voltage controller ( $G_{RU}$ ) and to the oscillating current controller ( $G_{RI}$ ), and carrying along the resultant controlling  
25 variable value ( $Y(t)$ ), if neither one of the controlling variable values ( $Y_{U(t)}$ ) and ( $Y_{I(t)}$ ) generated by their respective controllers is sent onward as the resultant controlling variable value ( $Y(t)$ ).

30           17. The method as of claim 13, further comprising sending onward as the resultant controlling variable value ( $Y(t)$ ) to the inverse rectifier circuit ( $G_{si}$ ), via the switching device, a controlling variable not lower than a  
35 predetermined minimum controlling variable value ( $Y_{min}$ ).

18. The method as of claim 14, further comprising  
sending onward as the resultant controlling variable value  
( $Y(t)$ ) to the inverse rectifier circuit ( $G_{si}$ ), via the  
switching device, a controlling variable not lower than a  
predetermined minimum controlling variable value ( $Y_{min}$ ).

19. The method as of claim 13, further comprising  
sending onward as the resultant controlling variable value  
( $Y(t)$ ) to the inverse rectifier circuit ( $G_{si}$ ), via the  
switching device, a controlling variable not higher than a  
predetermined maximum controlling variable value ( $Y_{max}$ ).

20. The method as of claim 14, further comprising  
sending onward as the resultant controlling variable value  
( $Y(t)$ ) to the inverse rectifier circuit ( $G_{si}$ ), via the  
switching device, a controlling variable not higher than a  
predetermined maximum controlling variable value ( $Y_{max}$ ).

21. The method as of claim 12, further comprising  
varying at least one parameter within at least one of the  
voltage controller ( $G_{RU}$ ) and the oscillating current  
controller ( $G_{RI}$ ), the at least one parameter being a  
function of at least one of a set x-ray tube voltage ( $U_{R0}$ )  
and a set x-ray tube current ( $I_{R0}$ ).

22. The method as of claim 14, further comprising  
varying at least one parameter within at least one of the  
voltage controller ( $G_{RU}$ ) and the oscillating current  
controller ( $G_{RI}$ ), the at least one parameter being a  
function of at least one of a set x-ray tube voltage ( $U_{R0}$ )  
or a set x-ray tube current ( $I_{R0}$ ).